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## ABSTRACT

We present the design and construction of a new experimental apparatus for the trapping of single  $\text{Ba}^+$  ions in the center of curvature of an optical-quality hemispherical mirror. We describe the layout, fabrication, and integration of the full setup, consisting of a high-optical access monolithic “3D-printed” Paul trap, the hemispherical mirror, a diffraction-limited in-vacuum lens ( $\text{NA} = 0.7$ ) for collection of atomic fluorescence, and a state-of-the-art ultra-high vacuum vessel. This new apparatus enables the study of quantum electrodynamics effects such as strong inhibition and enhancement of spontaneous emission and achieves a collection efficiency of the emitted light in a single optical mode of 31%.

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## I. INTRODUCTION AND MOTIVATION

Atomic ions confined and laser-cooled in Paul traps provide an experimental platform to study quantum objects with a unique level of control granted by the localization of the atomic wavefunction over a few nanometers, the long trapping time, and the high fidelity manipulation of internal and external degrees of freedom.<sup>1</sup> These features have been used extensively to build quantum information processors (see, for example, Ref. 2) and for the study of fundamental phenomena in quantum optics and atomic physics (see, for example, Ref. 3).

One of the most fundamental and intriguing phenomena in quantum optics is spontaneous emission and the possibility to modify it.<sup>4–7</sup> Spontaneous emission of atoms can be enhanced

or inhibited in several ways. One way to modify spontaneous emission rate is through dipole–dipole interactions between different atoms, namely, sub- and superradiance-type effects.<sup>8–11</sup> This has been extensively studied in neutral atom systems and used for diverse applications (see, for example, Refs. 12–20). In general, it is difficult to observe large modifications of spontaneous emission with trapped ions using this approach, since the Coulomb interaction restricts the minimum achievable inter-ion distance. Nevertheless, some degree of modification has been shown for the case of two ions. In Ref. 21, enhancement of  $\sim 1.5\%$  and inhibition of  $\sim 1.2\%$  were observed by locating two ions 1470 nm away from each other.

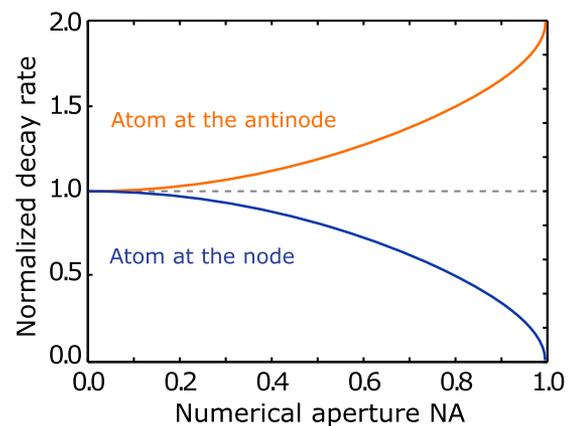
Another way to enhance or reduce spontaneous emission rate of an atom is to modify the electromagnetic vacuum mode structure interacting with the atom.<sup>22,23</sup> The electromagnetic mode

structure can be altered by placing the atom close to dielectric interfaces,<sup>24</sup> between two mirrors,<sup>25</sup> or inside photonic structures producing a bandgap.<sup>26</sup> In particular, large enhancement of emission from a single atom has been achieved using high-finesse cavities.<sup>27–30</sup> Recently, a fivefold enhancement in spontaneous emission rate has been demonstrated by placing a single atom in a fiber cavity.<sup>31</sup> Furthermore, in the realm of solid state emitters, enhancement by a factor of more than 100 has been observed using microcavities.<sup>32</sup> In ion trap systems, strong coupling between a single trapped ion and a fiber cavity has recently been observed.<sup>33</sup> While a resonant cavity can increase spontaneous emission rate into a particular mode, inhibiting spontaneous emission requires the suppression of the coupling to all modes. Only a few experiments have demonstrated large inhibitions (see, for example, Ref. 34 where the spontaneous emission rate of a single Rydberg atom was reduced by a factor of  $\sim 20$  or Ref. 35 where the emission rate of a solid state emitter was reduced by a factor of  $\sim 10$ ).

It is a common assumption in the field of cavity electrodynamics that full inhibition of spontaneous emission can only be achieved by placing the atom between mirrors that cover the full solid angle around it, restricting all the vacuum modes resonant with the atom (see, for example, Ref. 6). However, given the point symmetry of atomic emission, it is possible to fully control the emission rate by covering only *half* of the solid angle. This can be realized by placing the atom in the center of a concave hemispherical mirror, as theoretically predicted in Refs. 36 and 37. Taking this approach, both inhibition and enhancement of spontaneous emission can be achieved depending on the distance  $R$  between the atom and the surface of the mirror, provided that the mirror is close enough to the atom to allow the temporal interference of the field emitted in opposite directions. This condition can be written as  $2R/c \ll 1/\Gamma$ , where  $c$  is the speed of light and  $\Gamma$  is the free-space decay rate of the observed atomic transition. If  $R = n\lambda/2$ , where  $n$  is an integer and  $\lambda$  is the wavelength of the transition, an atom located in the center of curvature of the mirror is at a node of the vacuum mode density and inhibition is observed. Conversely, if the radius is  $R = n\lambda/2 + \lambda/4$ , an atom located in the center of curvature is at an anti-node of the vacuum mode density and enhancement is observed. If the mirror is not a hemisphere ( $NA = 1$ ), but a spherical mirror with  $NA < 1$ , only a partial modification is expected. Figure 1 shows the expected modification of the decay rate of a dipole transition depending on the numerical aperture of a perfectly reflective spherical mirror. Furthermore, in addition to the modification of spontaneous emission, a hemispherical mirror is predicted to lead to the ground and excited state level shifts.<sup>36,37</sup>

In this article, we present the new “Panopticon”<sup>38</sup> apparatus for the integration of a high-quality hemispherical mirror ( $NA \approx 1$ ) and a Paul trap in order to realize the situation described above. In addition to the fundamental components of such a setup, i.e., the hemispherical mirror and a Paul trap, a high numerical aperture lens ( $NA = 0.7$ ) is used to collimate light emission and direct it to a detector, as shown in Fig. 2. The design and construction of such an apparatus presents multiple technical challenges that are discussed in the following:

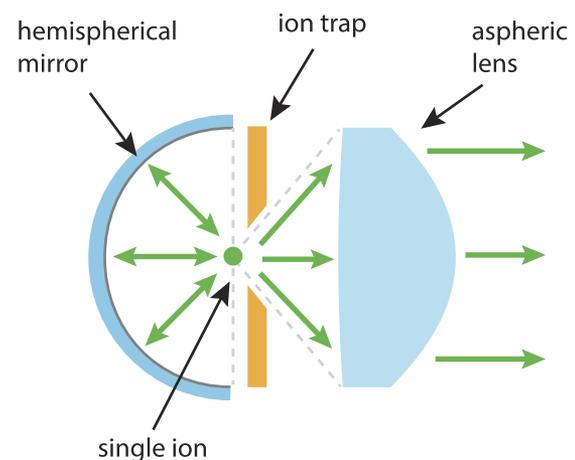
- In Sec. II A, we discuss the construction and characterization of the hemispherical mirror. The effects discussed above vanish rapidly when the mirror deviates from a perfect



**FIG. 1.** Modification of spontaneous emission rate of an atom in the center of a hemispherical mirror. Spontaneous emission of an atom at the center of curvature of a spherical mirror is inhibited or enhanced depending on the radius and numerical aperture of the mirror. If the radius of the mirror is  $R = n\lambda/2$ , the center of curvature is a node of the vacuum mode density and inhibition is expected (blue curve). If the radius of the mirror is  $R = n\lambda/2 + \lambda/4$ , the center of curvature is an anti-node of the vacuum mode density and enhancement is expected (orange curve). Full inhibition (respectively, a doubling of the decay rate) is obtained when half of the space is covered by the mirror ( $NA = 1$ ). In this plot, a mirror with perfect reflectivity is assumed.

hemisphere. The target rms surface error for the fabricated mirror is  $\lambda/10$  over the whole mirror surface. Furthermore, we describe how thermal expansion can be used to adjust the radius of the mirror in order to access both inhibition and enhancement of spontaneous emission.

- In Sec. II B, we discuss the design and characterization of the high-NA lens used for light collection. The lens design aims at diffraction-limited performance, enabling interference, and imaging experiments such as the ones presented in Refs. 39–41.



**FIG. 2.** Main components of the Panopticon setup. The green arrows show the propagation of the light emitted by the trapped atomic ion.

- In Sec. II C, we discuss the design of the Paul trap. The trap must provide full optical clearance between the trapped ion and the hemispherical mirror. Additionally, it must provide optical clearance for the high-NA lens and for the required laser beams. Ideally, the trap design should allow us to trap several ions simultaneously in a stable fashion and provide enough flexibility for multi-ion quantum optics experiments such as the one presented in Ref. 40.
- In Sec. II D, we discuss the integration of the mirror, trap, and lens. The position of the optical elements should be adjustable *in situ* with nanometer precision.
- In Sec. III, we present the design of the vacuum vessel. All the above-mentioned elements have to be placed in an ultra-high vacuum environment, which contains an atomic source and provides the required electrical connections and optical access.

Besides the fundamental interest in measuring effects predicted by quantum electrodynamics,<sup>36,37</sup> being able to control spontaneous emission of a dipole transition has several applications. For example, reducing the decay rate by two orders of magnitude on a dipole transition would increase the  $T_1$  time of the transition up to microseconds, allowing the implementation of a qubit on such a transition. Using a dipole transition would be beneficial because it permits fast qubit control without the use of strong laser beams. Another application can be found in laser cooling, as tuning the decay rate of a dipole transition would allow to directly modify, e.g., the Doppler cooling rate.<sup>42,43</sup> Furthermore, Doppler cooling typically needs repumper laser beams to depopulate additional states connected to the cooling transition.<sup>43</sup> By suppressing the spontaneous decay through these additional channels, it would be possible to Doppler cool without the need of repumping beams.

The system that we present here also provides high light collection efficiency. For an optimally oriented linear dipole, i.e., with its dipole moment oriented orthogonal to the optical axis used for collection, the expected single mode photon collection efficiency is 31.7%.<sup>44</sup> Remarkably, given the high quality of the overall optical system, with wavefront errors below  $\lambda/10$  for all the components, the collected light can be captured in a single mode and coupled efficiently to a single mode fiber. The high collection efficiency and the cleanness of the optical mode are expected to improve the signal-to-noise ratio of any optical measurement of atomic properties. Additionally, the improved collection and absorption rates enabled by this setup could be used to implement a quantum network without cavities.<sup>45,46</sup>

We note that some of the features exhibited by a setup employing a hemispherical mirror, such as high collection efficiency and improved single photon absorption, can be achieved using an atom in the focus of a parabolic mirror.<sup>47,48</sup> Indeed, in Ref. 48, collection efficiencies as high as 54.8% have been reported using a parabolic mirror. However, in this approach, the enhancement and inhibition of spontaneous emission due to QED effects vanish for macroscopic parabolic mirrors.<sup>47</sup> Other approaches consist in using a combination of a high-NA lens collecting the light emitted by an atom and a mirror that retro-reflects the collected light. Although changes in the decay rates have been observed using this method,<sup>49</sup> the modifications are limited by numerical apertures achievable in trapped ion systems for the collection lens. Furthermore, previous attempts to

position an ion in the center of a spherical mirror have demonstrated stable trapping and improved light collection,<sup>50</sup> but they have not achieved the mirror surface quality, radius tunability, and numerical aperture required to show inhibition or suppression of spontaneous emission.

## II. THE PANOPTICON SETUP

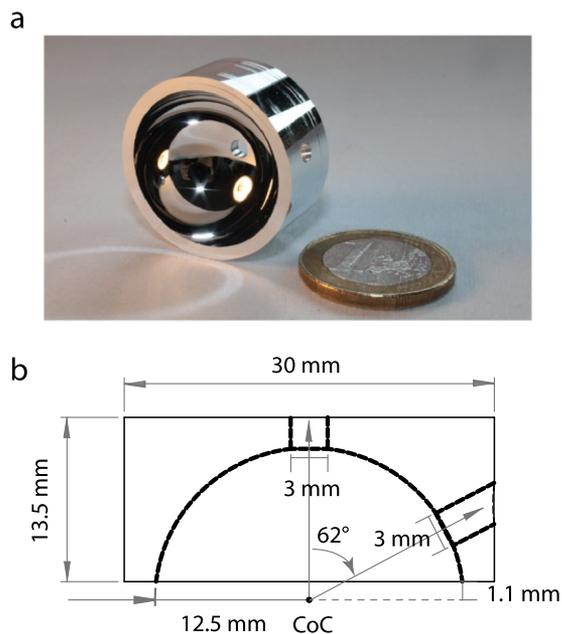
The main feature of the Panopticon setup is the ability to confine a single trapped atomic ion in the center of a hemispherical mirror. The ion trap needs to provide full optical access between the trapped ion and the mirror. Additionally, in order to capture a large portion of the emitted field, a high-NA aspheric lens ( $NA = 0.7$ ) is positioned opposite to the mirror such that its focal point lies at the position of the ion. Therefore, the trap also needs to provide optical access for the solid angle captured by the asphere. Figure 2 shows a schematic with the main components of the Panopticon setup. In Secs. II A–II D, we describe the design, construction, and characterization of each of these main components, as well as their integration and positioning.

### A. The hemispherical mirror

The main component of the Panopticon setup is the concave hemispherical mirror. The results about the fabrication and characterization of this mirror have been previously reported in Ref. 51. To observe a large modification of spontaneous emission of an atom located in its center, the surface of the mirror can deviate only minimally from that of a sphere over its full numerical aperture. To our knowledge, the most precise macroscopic spherical objects ever fabricated are spheres with a surface deviation of only 17 nm peak-to-valley.<sup>52</sup> This surface quality is achieved by randomly rotating the sphere between two polishing tools for periods of several days. Unfortunately, this technique cannot be applied to concave spherical surfaces, and in general, until now, there was no technique able to produce a surface precision similar to that of a convex sphere.

In collaboration with the Australian National University (ANU), we have produced hemispherical mirrors with rms form errors consistently below 25 nm, a maximum peak-to-valley error of 88 nm, and a radius of curvature  $\approx 12.5$  mm. The mirrors were fabricated by diamond turning from a cylindrical aluminum 6061 substrate using a CNC (computer numerical control) nano-lathe.<sup>53</sup> To achieve low surface errors, an *in situ* white-light interferometer was implemented on the lathe, permitting the calibration of the tool with sub-nanometer precision prior to the machining. A detailed description of the fabrication and characterization of the mirrors can be found in Refs. 51 and 54.

Figure 3 shows one of the fabricated mirrors, with a surface rms error of 18.1 nm ( $\lambda/27$  for  $\lambda = 493$  nm) and a peak-to-valley error of 116.5 nm estimated using stitch interferometry (see Ref. 51 for details). Two drilled holes (3 mm diameter) provide laser access to the center of curvature where the ion will be located (see Sec. II D). One of the holes is located along the optical axis of the mirror and the other at  $62^\circ$  with respect to the optical axis. The NA of the mirror is 0.996 (half aperture  $85^\circ$ ), which is not a limitation of the fabrication process and is chosen such as to provide 1.1 mm optical clearance to the trapped ion. This gives laser access orthogonal to the mirror's optical axis. The



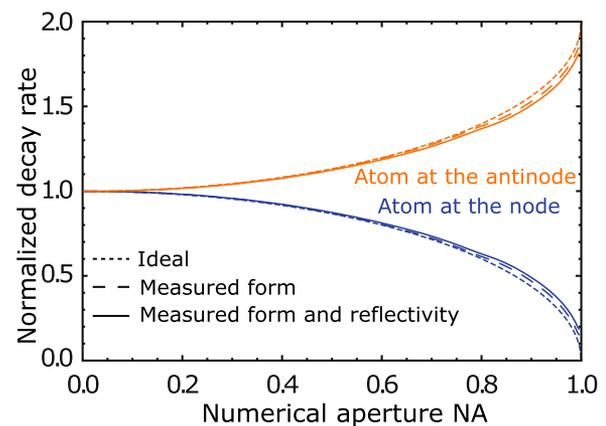
**FIG. 3.** Fabricated hemispherical mirror. (a) Photograph of a fabricated hemispherical mirror. A euro coin is used for comparison. (b) Schematic showing a cross section of the mirror with its relevant dimensions. Note that the 3 mm diameter drilled holes provide laser access to the center of curvature (CoC) of the mirror where the ion will be located. Reproduced with permission from Higginbottom *et al.*, "Fabrication of ultrahigh-precision hemispherical mirrors for quantum-optics applications," *Sci Rep* 8, 221 (2018). Copyright 2018 licensed under a Creative Commons Attribution (CC BY) license.

reflectivity of the mirror is set by the reflectivity of the substrate (0.92 for aluminum 6061 at 493 nm); it could be improved by applying a highly reflective thin film coating. However, the concave shape of the mirror makes it difficult to realize this in a uniform fashion, and special techniques would be required.<sup>55</sup> Figure 4 shows the expected modification of spontaneous emission considering the measured surface form, the reflectivity, and the effect of the drilled holes. Considering form and reflectivity, the maximum expected enhancement and inhibition of spontaneous emission rate in the 493 nm transition in  $^{138}\text{Ba}^+$  correspond to 88% of their ideal values. The main deviation from the ideal case comes from the limited reflectivity of the material.

The mirrors have been shown to be resilient to a cycle of vacuum bake-out under typical conditions (maximum temperature of 200 °C).

### 1. Temperature stabilization and tuning of the radius of curvature

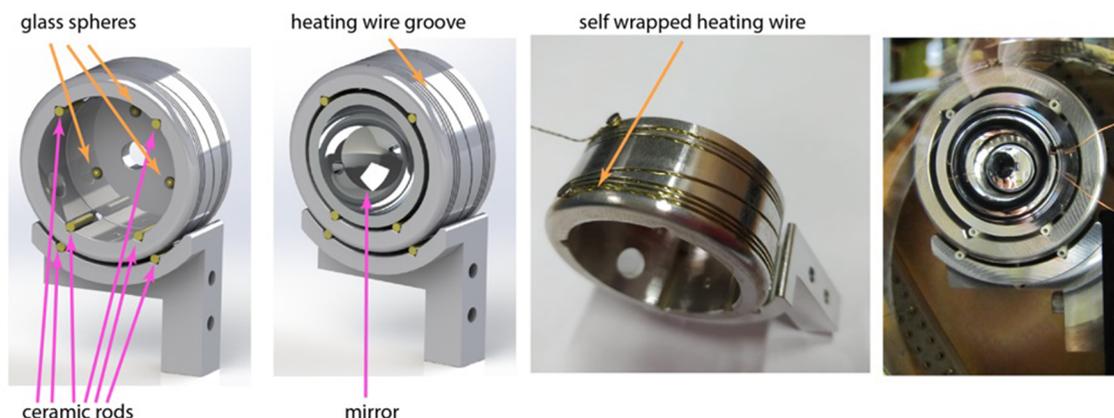
To tune the radius of curvature of the mirror, we rely on the uniform thermal expansion of the substrate. The coefficient of thermal expansion of aluminum 6061 at room temperature is  $23.5 \times 10^{-6} \text{ K}^{-1}$ .<sup>56</sup> A change in radius of curvature of  $\lambda/4 \approx 123.3 \text{ nm}$  (with  $\lambda = 493 \text{ nm}$ ) requires a temperature modification of 0.42 K. The mirror was heated when measured with a single-shot white-light ZYGO interferometer; this showed radius tunability over the desired



**FIG. 4.** Expected performance of the fabricated mirror. Modification of spontaneous emission rate considering the achieved form, and the achieved form and reflectivity of the substrate. The numerical aperture  $\text{NA} = 0.996$  is not distinguishable from  $\text{NA} = 1.0$  in the plot. Considering form and reflectivity, the maximum expected enhancement and inhibition of spontaneous emission rate correspond to 88% of the ideal value.

range with no measured surface distortion due to thermal expansion. Nevertheless, small variations in environmental temperature in the experiment may lead to the drifts of the radius of curvature; therefore, active stabilization of the temperature of the mirror is necessary.

To control and stabilize the temperature of the mirror, we designed a resistively heated holder, as shown in Fig. 5. The holder is heated by applying current to a self-wrapped heating wire.<sup>57</sup> The total resistance of the heating wire is 65  $\Omega$ , and the current applied varies between 0.1 A and 0.2 A depending on the set temperature. The temperature of the holder is measured in the back of the holder using two temperature sensors,<sup>58</sup> which are glued to the holder.<sup>59</sup> The mirror is not in direct contact with the holder, it lies on ceramic rods<sup>60</sup> and glass spheres<sup>61</sup> (see Fig. 5), providing a distance of 1.1 mm between the outer surface of the mirror and the inner surface of the holder. This reduces the contact thermal conductivity between the mirror and the holder while maintaining the radiative heat transfer and provides a homogeneous temperature over the volume of the mirror, albeit with a slow temperature tuning rate. The temperature is stabilized with a feedback loop using a high-precision proportional integral differential controller (PID).<sup>62</sup> In-vacuum tests have shown mirror temperature fluctuations below 1 mK over 10 h for different set points between 293 K and 303 K. The heating time constant of the mirror has been measured to be 5.39 h, while the cooling time constant (cooling is achieved passively) is 3.89 h. These times may be reduced by increasing the thermal contact between the mirror and the holder, which would, however, lower the temperature stability. The PID can be operated in the sample and holder or constant current regime, which is useful for sensitive atomic measurements where a constant magnetic field could be required. The achieved temperature stability corresponds to fluctuations in the mirror's radius of curvature below 20 nm, which are lower than the measured surface error of the mirror. As mentioned above, the mirror is grounded. This is done to avoid any charging that could affect the trapping potential. The grounding is done with a thin (25  $\mu\text{m}$



**FIG. 5.** Mirror holder and heater. Components of the mirror's aluminum holder and heater used to achieve a mirror temperature stability below 1 mK. The right-most panel shows the setup used during the temperature stability tests performed in vacuum, with a thermistor attached directly to one of the mirrors.

diameter) gold wire in the front side of the mirror, fixed with conductive epoxy. The grounding wire has a negligible effect in the temperature stability and heating and cooling constants.

### B. The aspheric lens

To capture and collimate the light emitted by the ion, an aspheric lens is located opposite to the hemispherical mirror, as shown in Fig. 2. The main advantages of using an aspheric lens instead of a multi-lens objective are the simple, compact design, and the reduced spherical and other optical aberrations. A low-aberration optical system is a crucial requirement for future experiments related to the spatial properties of emitted and absorbed photons for interference experiments with photons emitted by atoms in different traps coupled with optical fibers.

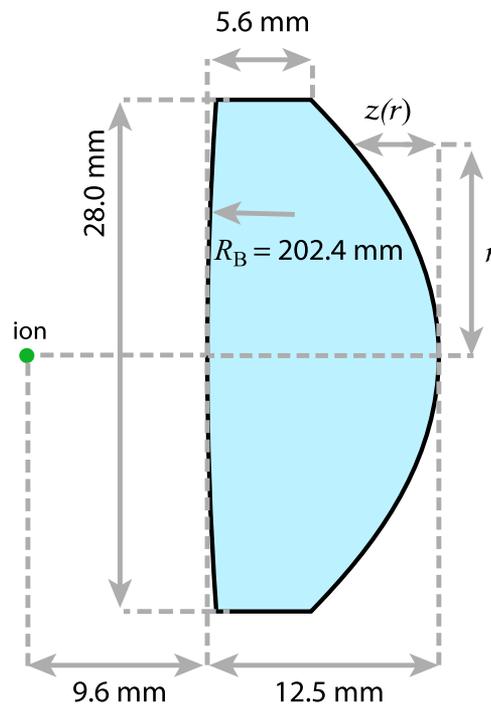
The asphere, designed and fabricated by Asphericon GmbH, has an NA = 0.7, a working distance of 9.60 mm, and an effective focal length of 16.05 mm. The design was optimized using Zemax OpticStudio to achieve a diffraction-limited performance with ultra-low wavefront aberrations at 493 nm. The dimensions of the designed asphere are shown in Fig. 6. The surface facing the ion has a designed constant radius of curvature  $R_B = 202.353$  mm, whereas the opposite surface is a rotation symmetric asphere defined by the following equation:

$$z(r) = \frac{r^2}{R_F \left( 1 + \sqrt{1 - (1+k) \frac{r^2}{R_F^2}} \right)} + \sum_{i=2}^8 A_{2i} r^{2i}. \quad (1)$$

The values of parameters  $R_F$ ,  $k$ , and  $A_{2i}$  are listed in Table I.

Three pieces of the designed asphere were fabricated using a S-TIH53 glass substrate<sup>63</sup> with the refractive index  $n_g \approx 1.87$  ( $\lambda = 493$  nm) and the Abbe number  $v_g = 23.59$  ( $\lambda = 546$  nm). The manufacturing process includes CNC grinding and polishing as a first step. Thereafter, ion beam figuring is used to reduce surface irregularities.<sup>64</sup> In this process, ion beams are directed at specific regions of the surface where surface errors have been detected.

Finally, an anti-reflective coating for 493 nm is applied using plasma-assisted physical vapor deposition.<sup>65</sup> All these steps were performed by Asphericon GmbH. Figure 7(a) shows a photograph of one of the aspheres, and Fig. 7(b) shows the measured wavefront distortion.<sup>66</sup> rms wavefront distortions below 37 nm ( $\lambda/14$ ) and peak-to-valley distortions below 700 nm over the full numerical aperture were



**FIG. 6.** Aspheric lens dimensions. The surface facing the ion is spherical with a radius of curvature  $R_B$ , whereas the aspheric surface is defined by Eq. (1). The ion is positioned 9.6 mm away from the front surface. The aspheric surface design parameters are listed in Table I.

TABLE I. Aspheric lens design parameters.

Parameter	Value
$R_F$	14.56 mm
$k$	-0.776
$A_4$	$3.202\,280\,6 \times 10^{-6} \text{ mm}^{-3}$
$A_6$	$-2.900\,266\,1 \times 10^{-8} \text{ mm}^{-5}$
$A_8$	$-9.624\,991\,0 \times 10^{-11} \text{ mm}^{-7}$
$A_{10}$	$-1.023\,645\,6 \times 10^{-13} \text{ mm}^{-9}$
$A_{12}$	$4.551\,145\,9 \times 10^{-16} \text{ mm}^{-11}$
$A_{14}$	$3.320\,125\,2 \times 10^{-18} \text{ mm}^{-13}$
$A_{16}$	$-8.764\,529\,8 \times 10^{-21} \text{ mm}^{-15}$

achieved for the three aspheres. From Fig. 7(b), it is clear that the largest wavefront distortions occur close to the lens edge. In fact, by reducing the aperture of the lens to  $NA = 0.65$ , the rms wavefront error is reduced to  $\lambda/24$ . The reflection from each coated surface was measured to be smaller than 0.4% for incidence angles up to  $40^\circ$ , and the on-axis transmission of the lens was  $\approx 95\%$ , in agreement with the expected values. Both measurements were done with a laser beam with a 493 nm wavelength.

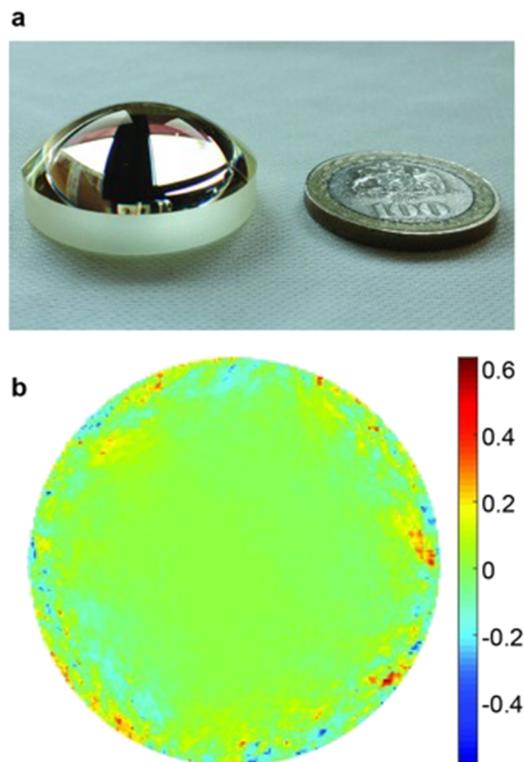


FIG. 7. Fabricated aspheric lens. (a) Photograph of one of the three fabricated aspheric lenses together with a hundred Chilean pesos coin, giving the scale (the coin has a diameter of 23.25 mm). (b) Measured wavefront distortion of one of the aspheres. Numbers in the color scale are in units of  $\lambda = 493$  nm. Provided by Asphericon GmbH.

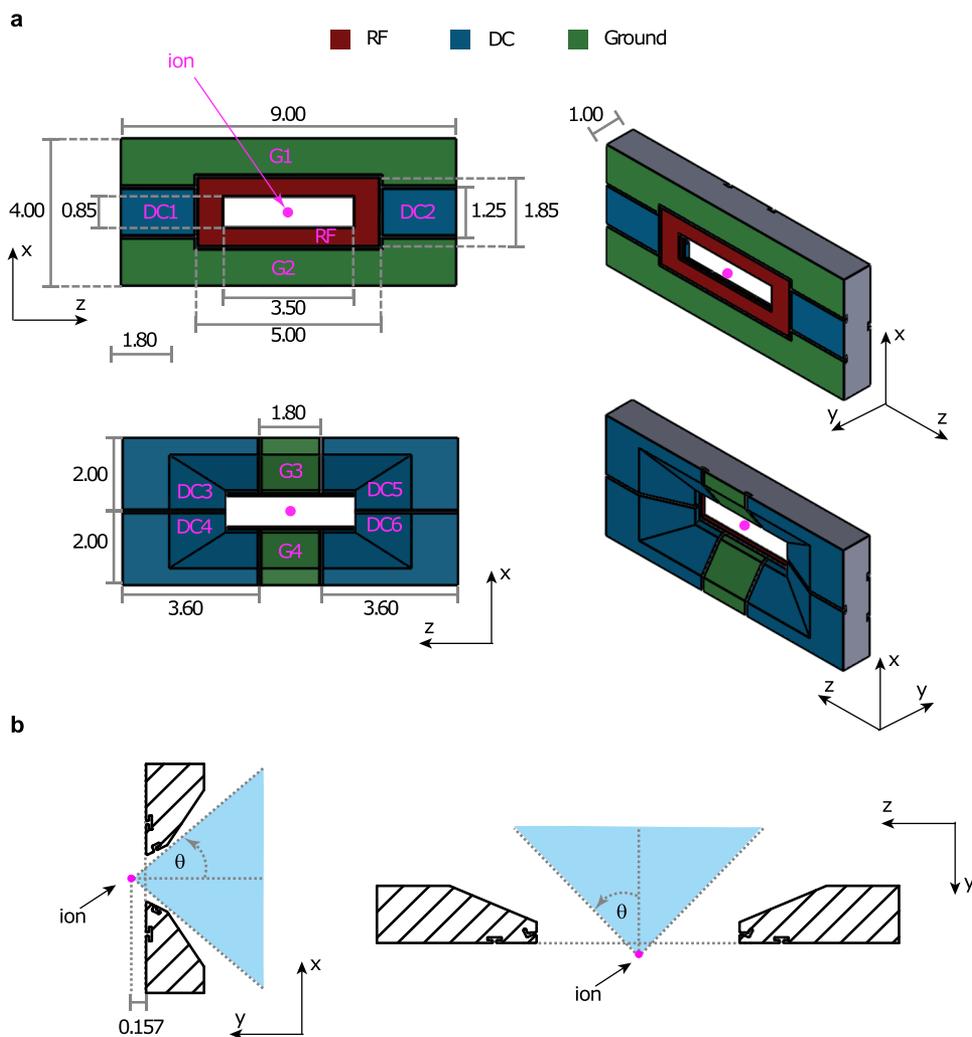
The lens is mounted in an aluminum holder, which allows for laser access to the focal point of the lens from several directions (see Sec. II D), and with negligible reduction in the numerical aperture.

### C. The ion trap

The main challenge in the design of an ion trap compatible with the Panopticon setup is that the trap should provide full optical access not only between the trapped ion and the hemispherical mirror but also between the ion and the aperture defined by the aspheric lens. This could be achieved using, for example, a needle trap.<sup>67</sup> However, this approach allows the trapping of only one ion without excess of micromotion and displacement of the trapped ions. It is desirable to be able to trap several ions without micromotion, since the setup could then be used for a broader range of quantum optics experiments. Some comply partially with the criteria for optical access and stable trapping of several ions, including, for example, the miniaturized segmented “High Optical Access Trap 2.0” developed by the Sandia National Laboratories.<sup>68</sup> However, this trap only possesses a clear aperture equivalent to  $NA = 0.25$ . The approach that we take here is the fabrication of a monolithic slotted pseudo-planar macroscopic trap. A simplified scheme of the trap geometry, with only the minimal electrode configuration needed to trap an ion, is shown in Fig. 8. Later in this article, we discuss the actual fabricated trap with additional features. In the design, an ion is trapped above the front surface, providing full clearance on the side of the hemispherical mirror and, through the slot, clearance corresponding to the numerical aperture  $NA = 0.7$  of the aspheric lens. The geometry shown in Fig. 8 generates a confining RF pseudo-potential in the  $x$  and  $y$  directions, whereas trapping along the  $z$  direction is provided by the DC potential generated primarily by the DC electrodes DC1 and DC2. The DC voltages applied to the electrodes DC3, DC4, DC5, and DC6 contribute weakly to the trapping potential in the  $z$  direction and are meant for micromotion compensation. The ring shape of the RF electrode, although counter-intuitive, is the result of systematic optimization, starting from two  $\pi$ -shaped separated RF electrodes producing a cross-shaped slot (see Fig. 9), varying the dimensions of the slot, and keeping a fixed slot vertical (along  $x$ ) aperture. The obtained shape with a rectangular slot exhibits a reduced residual axial ( $z$  direction) pseudo-potential, allowing chains of  $\sim 20$  ions to be trapped with negligible axial micromotion.

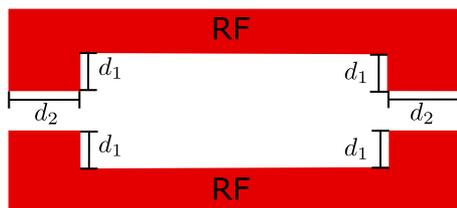
The fabrication is done with subtractive 3D laser micro-machining technology. The basic idea is to laser-machine a monolithic dielectric substrate to the required shape, including “trenches” separating different regions. In the following, we will refer to this technique as “3D-printing.” The surfaces are then coated with gold, creating an independent electrode in each region surrounded by trenches. Figure 10 depicts how 3D-printing and coating are combined to create electrodes without the need for shadow masking and reduce the number of angled metal evaporation steps needed. The bottom of the carved trenches can be grounded or connected to one of the contiguous electrodes by shaping “ramps” between the bottom and the surface in the 3D-printing design.

The required precision of the dielectric substrate fabrication can be achieved by “laser carving” techniques provided by companies such as FEMTOprint S.A. in Switzerland or Translume Inc. in USA. The 3D-printing technology used by these companies employs



**FIG. 8.** Ion trap design. (a) Simplified design of the trap. The RF, DC, and ground (G) electrodes lie on the facets of a 3D-printed substrate. All dimensions in mm. Pink text indicates electrode names. (b) Transverse cuts of the trap showing the optical clearance. The trap design provides full clearance toward the hemispherical mirror ( $y > 0$ ). On the other side ( $y < 0$ ), the optical clearance is slightly larger than required by the aspheric lens with  $NA = 0.7$ , corresponding to a  $\theta = \arcsin(NA) \approx 44.4^\circ$  opening angle (blue area). The RF pseudo-potential minimum, and therefore the position of the ion, is located at a distance  $y = 0.157$  mm from the front plane of the trap.

strongly focused high-energy laser pulses to locally change the physical structure of the substrate. A chemical process is then used to remove the treated material. Using this technique on, e.g., fused silica, the carved features can reach an average surface roughness below 100 nm, whereas the untouched surfaces can reach an average roughness below 5 nm. Additional polishing can reduce the



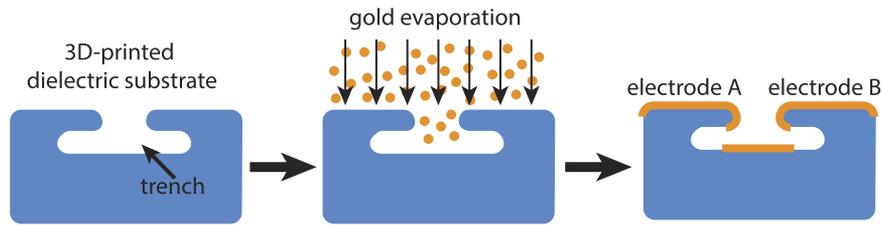
**FIG. 9.** Slot shape optimization. The ring shaped RF is the result of optimization starting from two separated  $\pi$ -shaped RF electrodes and varying the lengths  $d_1$  and  $d_2$  while keeping the other dimensions of the electrode fixed.

roughness below 50 nm, though with detrimental effects in the surrounding areas. The scale of the surface roughness achieved has been demonstrated to be adequate for use in ion traps with a minimum ion-electrode distance of  $\sim 100 \mu\text{m}$  (see, for example, Ref. 69), whereas in our trap that distance, as described below, is  $453 \mu\text{m}$ . A more detailed description of this fabrication technology applied to the fabrication of ion traps can be found in Ref. 69.

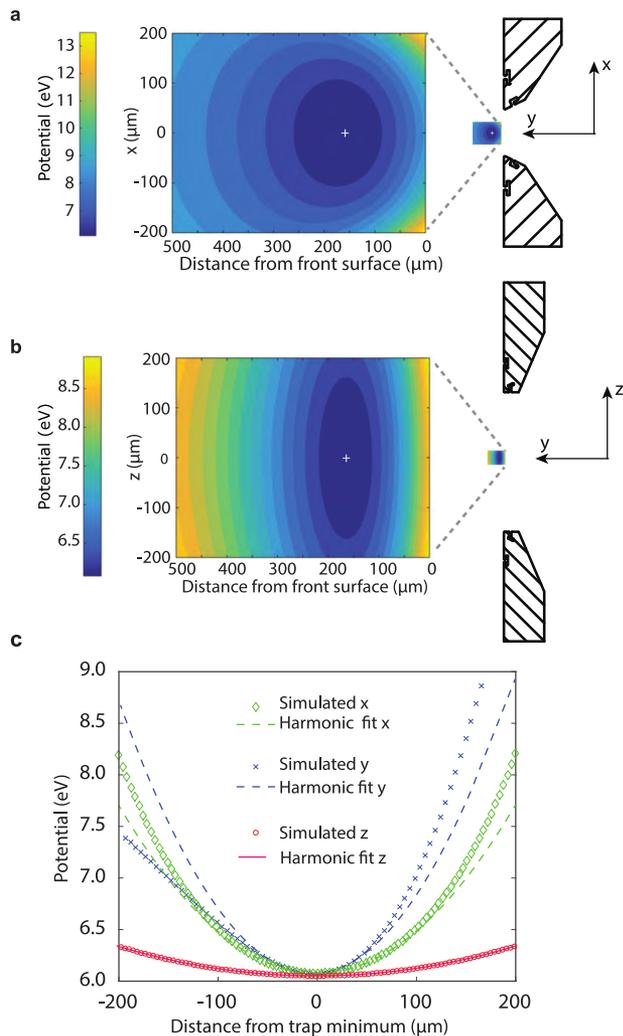
The conductive coating is applied in our clean room by means of electron beam evaporation of a thin layer of titanium ( $\sim 2$  nm), used as an adhesion layer, followed by a thick layer of gold ( $\sim 200$  nm). Gold evaporation is applied from three different angles on each side of the substrate. Gold electroplating could also be used afterward to increase the thickness of the electrodes to  $\sim 5 \mu\text{m}$ .

### 1. Simulations of the trapping potential

The trap geometry presented in Fig. 8 is the result of a systematic optimization. The different dimensions and positions were varied to maximize the trapping frequencies for a  $^{138}\text{Ba}^+$  ion, as well as the trap depth, and to reduce the trap capacitance and the residual



**FIG. 10.** Electrode fabrication through 3D-printing and coating. First, a dielectric substrate is “3D-printed” to create the trenches needed to separate electrodes. Then, the surfaces are coated with a conductor (gold) in an evaporation step. The profile of the trenches combined with the directionality of the evaporation step provides electric insulation between different regions, defining trap electrodes. The recess in the profile allows us to apply evaporation from different angles without shorting the electrodes. The dimensions of the trench profile chosen for the fabricated trap are shown in Fig. 12(d).



**FIG. 11.** Simulated trapping potential. The parameters are those of “config. 1” in Table II. (a) Cross section through the  $x$ - $y$  plane. The white cross shows the position of the minimum. (b) Cross section through the  $y$ - $z$  plane. (c) Trapping potential along the  $x$ ,  $y$ , and  $z$  axis. Close to the center, in a range of  $\pm 50 \mu\text{m}$ , the potentials are well approximated by harmonic potentials.

axial RF field. The ion-electrode distance, which is constrained by the required optical clearance and laser access to the ion, was maximized. The electric potentials produced by the trap electrodes were simulated via finite element analysis using the software COMSOL Multiphysics 4.4. In these simulations, the grounded hemispherical mirror was included.

Figure 11 shows the total trapping potential. The RF pseudo-potential minimum is located  $157 \mu\text{m}$  away from the front plane of the trap, and the distance of a trapped ion to the closest electrode is  $453 \mu\text{m}$ . For comparison, in our current “Innsbruck-style” blade trap,<sup>70</sup> this distance is  $707 \mu\text{m}$ . Small ion-electrode distances tend to increase the ion heating rate due to, e.g., surface noise.<sup>71</sup> Keeping this distance relatively large is therefore important.

Figure 11(c) shows the trapping potentials along each coordinate axis. The potential is symmetric about the trap center along directions  $x$  and  $z$ , but not along  $y$ , as typically observed in surface traps.<sup>57</sup> The trapping frequencies can be varied with the voltages applied to the different electrodes. Table II shows the simulated trapping frequencies and trap depths obtained for a  $^{138}\text{Ba}^+$  ion. The trap depths are in the eV regime, comparable to 3D rod or blade traps,<sup>72</sup> which makes the trap suitable for operation at room temperature.

Simulations show that independent control of the voltages applied to the electrodes DC3, DC4, DC5, and DC6 is sufficient

**TABLE II.** Trap driving parameters and resulting trap frequencies and depths, obtained by finite-element simulations for  $^{138}\text{Ba}^+$ . Three different configurations are shown. DC1 and DC2 refer to the “endcap” electrodes shown in Fig. 8, while DC3, DC4, DC5, and DC6 are the electrodes in the back plane. In these three configurations, the electrodes G1, G2, G3, G4, and the mirror are grounded.

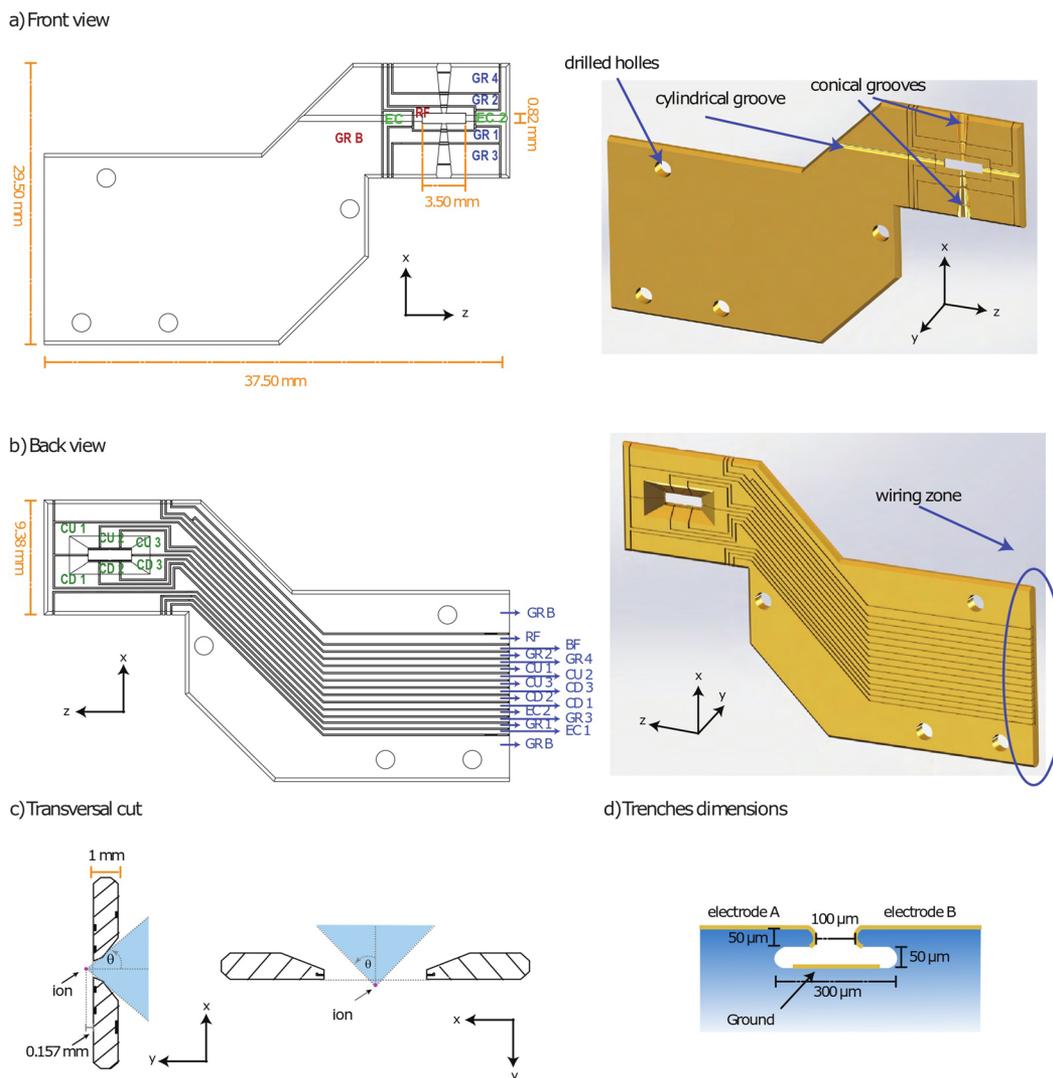
	Config. 1	Config. 2	Config. 3
RF freq. $\Omega_{\text{RF}}/2\pi$ (MHz)	16.0	16.0	16.0
RF amplitude $U_{\text{RF}}$ (V)	1000	1500	2000
DC1,2 (V)	200	300	400
DC3,4,5,6 (V)	82	123	164
$\omega_x/2\pi$ (MHz)	1.33	2.16	2.96
$\omega_y/2\pi$ (MHz)	1.57	2.34	3.07
$\omega_z/2\pi$ (MHz)	0.51	0.62	0.72
Trap depth (eV)	2.4	4.9	8.2

for compensation of micromotion in all directions. Further simulations with different trench geometries and dimensions were carried out. The most relevant trench parameter, i.e., the electrode-electrode separation provided by the trench, was varied between  $50\ \mu\text{m}$  and  $150\ \mu\text{m}$ . Variations in this range have a negligible effect on the trapping potential so that the final dimensions were selected based on the breakdown test results described in Sec. II C 2.

## 2. The fabricated trap

While the fabricated trap has the same core geometry as presented in Fig. 8, it includes additional features. Figure 12 shows the schematics and renders of the actual design. The ground electrodes

G1 and G2 in the front plane are divided into smaller electrodes GR1, GR2, GR3, and GR4 [Fig. 12(a)] to add control of the RF potential minimum position while keeping micromotion compensated, allowing the possibility of moving the ion in any direction several micrometers. These electrodes, together with all other electrodes in the front plane (EC1, EC2, RF, and GRB), are extended to reach the back plane. There, together with the back plane electrodes CU1, CU2, CU3, CD1, CD2, and CD3, they are prolonged into conductive traces extending beyond the radii of the hemispherical mirror and of the aspheric lens [Fig. 12(b)]. This flat and elongated design provides enough space for wire-bonding, which connects the electrodes to the voltage supplies through a printed circuit board (PCB, see Sec. II C 3). In this way, the optical clearance to the



**FIG. 12.** Full design of the ion trap. (a) Front side of the final trap design. Cylindrical and conical grooves are carved in the substrate in order to minimize the scatter of laser beams propagating close to the surface. All front electrodes extend to the back plane via the edges of the trap. (b) In the back plane, all the electrodes are extended to one extremity of the substrate, where wire-bonding is used for connection to voltage supplies. (c) Transverse cut at the trap center showing the optical clearance provided by the trap. (d) Dimensions of the trenches separating the electrodes.

trapping region is not affected by the bonding wires. The extended area is also used to mount the trap to an aluminum holder using through-holes.

Additionally, grooves in the front face are carved in the substrate (during the 3D-printing process). These grooves improve the clearance of the laser beams that propagate close to the surface, reducing the light scattered by the trap. This is of particular importance when addressing single ions using a strongly focused  $1.7\ \mu\text{m}$  laser. The conical vertical grooves shown in Fig. 12(a) match the divergence of such a beam with additional  $100\ \mu\text{m}$  clearance from the point where the beam intensity has decayed by a factor of  $1/e^2$ . The horizontal cylindrical grooves give enough optical clearance for lightly focused axial cooling and optical pumping beams. Figure 12(c) shows transverse cuts at the trap center, showing the position of the ion and the optical clearance provided by the design. The dimension of the trenches separating adjacent electrodes, shown in Fig. 12(d), was chosen after performing in-vacuum DC and RF breakdown tests on a simplified trap. The separation between electrodes varied between  $50\ \mu\text{m}$  and  $150\ \mu\text{m}$ . These tests did not show any sign of electric breakdown between electrodes with DC voltages as high as  $700\ \text{V}$  and RF voltages as high as  $1200\ \text{V}$  at  $20\ \text{MHz}$ . The separation was finally chosen to be  $100\ \mu\text{m}$ . The bottom of the trenches is connected to the common ground GR B. A complete 3D drawing of the designed trap can be found in the supplementary material. Figure 13 shows a photograph of one of the traps fabricated by FEMTOprint S.A. before metalization.

We have performed simulations of the generated trapping potential for the fabricated trap design, including all the aforementioned features. The differences with the results of the simulations of the simplified version presented in Sec. II C 1 are negligible.

### 3. Trap holder, in-vacuum low-pass filter, and voltage driving

The ion trap is mounted on an aluminum holder plate ( $2\ \text{mm}$  thickness) using three screws, as shown in Fig. 14(a). The holder plate also acts as a heat sink for the trap and is contacted to the body of the vacuum chamber. This plate also holds a filter PCB. The trap is wire-bonded to the PCB using gold wires. The PCB, made of alumina<sup>73</sup> with a thickness of  $1\ \text{mm}$ , has 16 silk-printed gold traces, wire-bond pads, paths, and soldering pads<sup>74</sup> for DC and RF routing. There are eight vias to route some of the paths to the opposite side of the PCB. All the DC paths are capacitively coupled to a common ground using  $1\ \text{nF}$  high-voltage surface mounted capacitors,<sup>75</sup> suppressing RF pick up. Additionally,  $1\ \text{k}\Omega$  ex-vacuum resistors are used in order to filter high frequency noise induced in the DC electrodes (cutoff frequency  $1\ \text{kHz}$ ). Figures 14(b) and 14(c) show a schematic

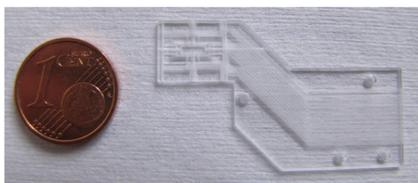


FIG. 13. Fabricated ion trap. Fabricated ion trap before metalization.

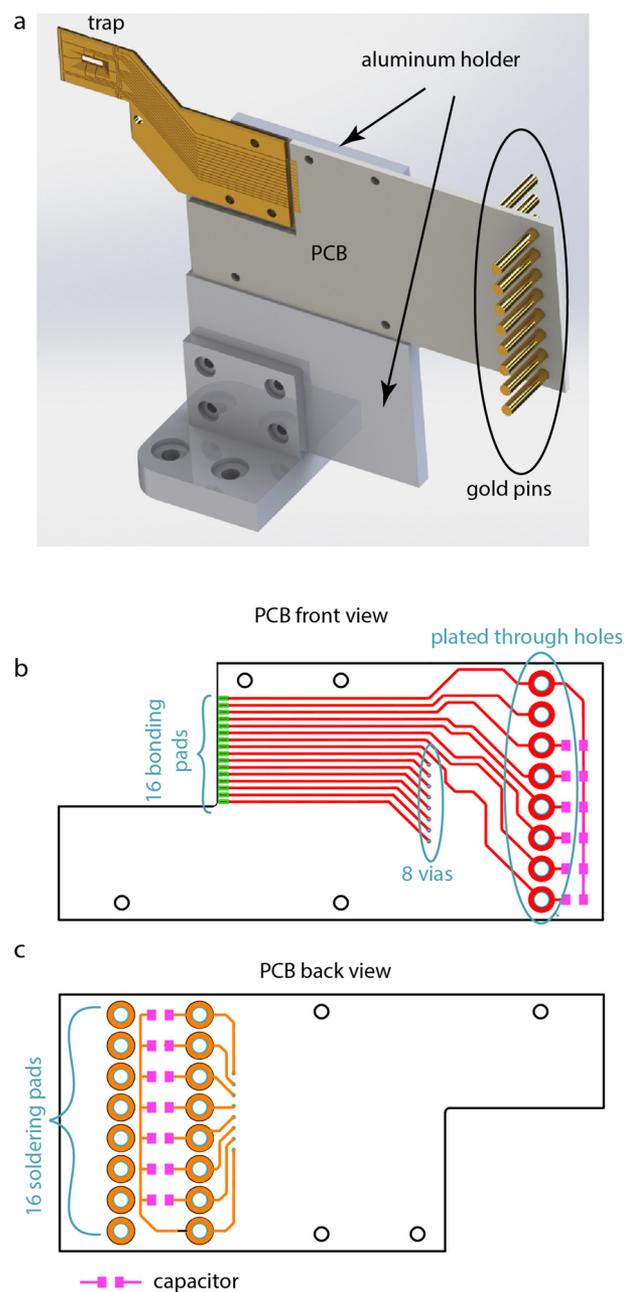


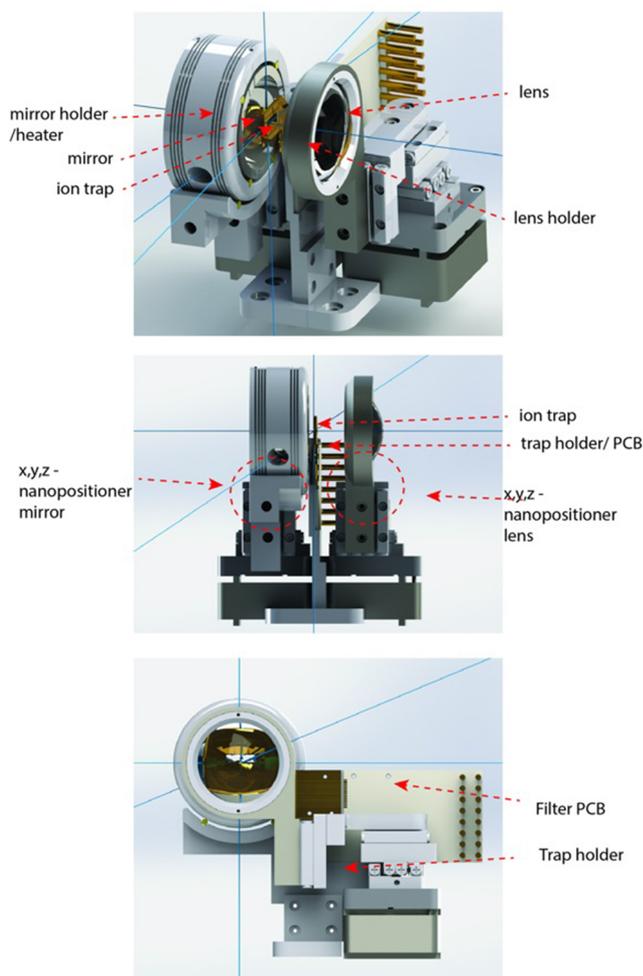
FIG. 14. Trap holder and filter PCB. (a) Both the trap and the PCB filter are mounted on an aluminum holder. The trap is wire-bonded to the PCB, which has conducting paths, capacitors, and pins for connection to the DC and RF sources. (b) and (c) Details of the PCB paths, position of the capacitors, and pins.

view of the PCB. At the edge opposite to the trap, the PCB has 16 gold pins<sup>76</sup> soldered,<sup>77</sup> allowing easy connection and disconnection of each line to copper wires attached to the electrical feedthroughs on the base vacuum flange (Fig. 16). None of the PCB traces or the wires are exposed to the atomic flux from the atom source (see Sec. III A).

The DC voltages are generated outside the vacuum chamber using a high-precision high-voltage source.<sup>78</sup> The RF voltage is generated using a high-precision signal generator<sup>79</sup> followed by a 28 dB amplifier<sup>80</sup> and a helical resonator.<sup>81</sup>

#### D. System integration

The optical setup, consisting of the hemispherical mirror, the aspheric lens, and the ion trap, has to be set in place in a robust and stable manner while still providing enough degrees of freedom for correct alignment. The holders and positioners have to be compatible with the ultra-high vacuum environment needed to trap single atomic ions in a stable way. To do so, we designed the mounting system shown in Fig. 15. In this setup, all the elements are carefully designed in order to provide the optical clearance required by the mirror and the lens, and laser access. The positions of the mirror and the lens can be set independently using *xyz*-nanopositioners<sup>82</sup>



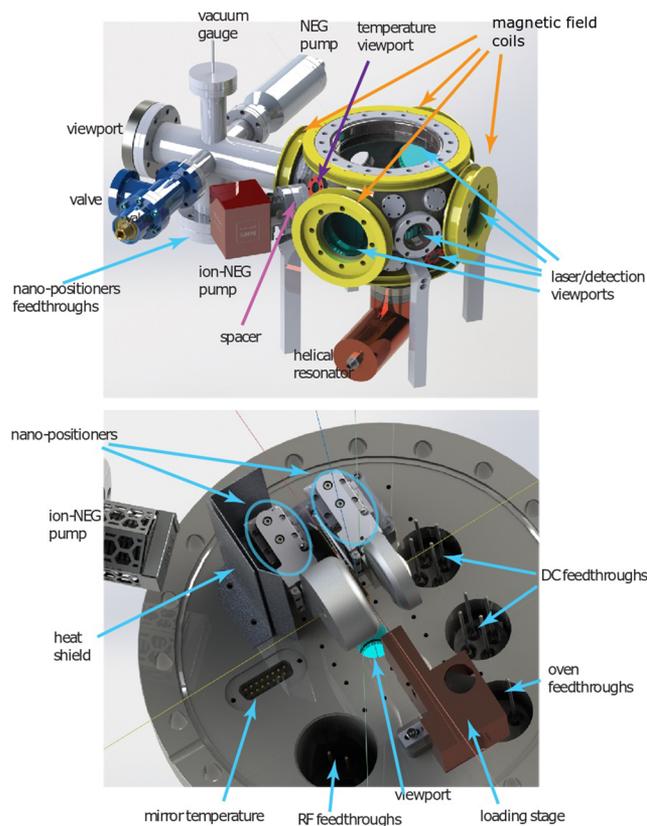
**FIG. 15.** Panopticon optical setup. The mirror and lens are mounted on independent *xyz*-nanopositioners, whereas the position of the ion trap is fixed. The blue lines show the four laser axes.

shown in this figure. The positioners have a step size of 1 nm in each direction, a position readout resolution of 1 nm, and a maximum displacement of 12 mm.

#### III. THE VACUUM VESSEL

The Panopticon optical setup is placed in an ultra-high vacuum environment. The vacuum vessel, shown in Fig. 16, is built around an 8 in.-CF spherical octagon chamber.<sup>83</sup>

A customized 6-way cross is attached to the main chamber, providing enough flanges to connect a vacuum valve,<sup>84</sup> a vacuum gauge,<sup>85</sup> the electric feedthroughs for the wiring of the nanopositioners, a non-evaporable getter (NEG) pump,<sup>86</sup> and a viewport. The main pumping is done with a combined ion and a NEG pump<sup>87</sup> attached to the main chamber. During the NEG activation, the pump can reach temperatures close to 450 °C. This temperature is not compatible with the maximum temperature to which the nanopositioners can be exposed (150 °C). In order to avoid damaging the nanopositioners, the pump is retracted from the main chamber using a spacer, and a two-layer aluminum heat shield is placed between the pump and the positioners (see Fig. 16). According to finite-element simulations performed by the pump manufacturer, this is sufficient to prevent damage of the nanopositioners. We plan to perform additional test to confirm this predictions, and if necessary, the shielding and the pump position will be modified.



**FIG. 16.** Main components of the vacuum vessel (see details in the main text).

The vacuum vessel has all the necessary viewports to provide laser access to the center of the trap using the planned beam directions (see Fig. 15), including a CF-160 viewport on top of the chamber. All the viewports<sup>88</sup> are anti-reflection coated for all the wavelengths needed to load, cool, and control  $^{138}\text{Ba}^+$  ions, i.e., 413 nm, 493 nm, 614 nm, 650 nm, and 1762 nm. For these wavelengths, the reflectivity is below 1%. The viewport used for transmitting the light emitted by the ion and collimated by the aspheric lens has an optical quality surface, with wavefront aberrations below  $\lambda/10$  over all the surface (with  $\lambda = 493$  nm).<sup>89</sup> An additional Germanium viewport<sup>90</sup> is attached to the main chamber, to allow monitoring of the temperature of the atom oven using a thermal camera outside the chamber (see Sec. III A).

The electrical connections needed to drive the ion trap, to heat an atom dispenser oven, and to measure and control the temperature of the mirror are routed through feedthroughs in the customized CF-160 bottom flange, assembled by Vacom GmbH (Fig. 16). This flange has a SUB-15 feedthrough for all the mirror temperature stabilization connections, a two-wire (12 kV, 13 A) feedthrough for the oven connections, two four-wire (12 kV, 13 A) for the trap DC connections, and a 2-wire (5 kV, 25 A) for the RF trap connections. This customized flange has also a CF-16 viewport intended for 1.7  $\mu\text{m}$  laser addressing of individual trapped ions. The connections for the nano-positioners are in one of the arms of the cross.

### A. Atom source

To provide a source of atoms inside the vacuum chamber, we have designed a loading stage that simultaneously contains a resistively heated Ba dispenser oven and a laser ablation target. The resistively heated oven is a reliable way to produce a flux of neutral atoms in the center of the trap, which can then be ionized using a 413 nm laser through a two-step excitation process.<sup>70</sup> This process is, however, slow and produces an excess of heat inside the vacuum chamber that can have detrimental effects on the operation of ion traps, such as undesired thermal expansion of the electrodes and thermal expansion of the hemispherical mirror.

Laser ablation from a target is an alternative method, which has been proved to be more efficient and less detrimental to ion trap operation (see, for example, Ref. 91). In this approach, short and strong laser pulses are applied on a Ba target to produce neutral and ionized atoms, which eventually reach the center of the trap. It has been experimentally shown that instead of using a pure Ba target, targets containing  $\text{BaTiO}_3$  or  $\text{BaO}$  produce higher  $\text{Ba}^+$  yields,<sup>92</sup> making loading more efficient while lifting the requirement of an additional photo-ionization laser. At the same time, using  $\text{BaTiO}_3$  instead of pure Ba, prevents fast oxidation of the sample during preparation of the vacuum setup. To guarantee isotope-selective loading, we still plan to use photo-ionization of ablated neutral atoms.

Figure 17 shows the designed loading stage, where both a resistive dispenser oven<sup>93</sup> and a  $\text{BaTiO}_3$  ablation target<sup>94</sup> are located. The holder is made of macor<sup>®</sup> ceramic, which exhibits a low thermal and electric conductance. Both the target and the oven are enclosed in a copper shield, which simultaneously acts as a thermal radiation shield and prevents the ablated Barium from coating surfaces in the

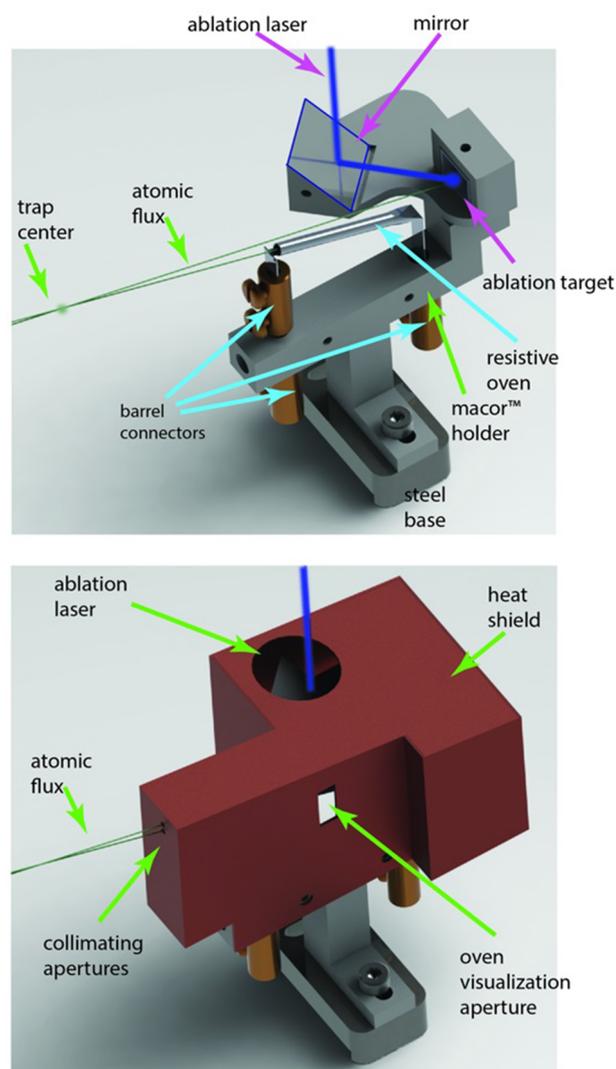


FIG. 17. Loading stage. Design of a loading stage combining a resistive Barium dispenser oven and a target for laser ablation (see details in the main text).

chamber and in the trap. Two circular apertures in the front with 1 mm diameter, one for each atom flux production process, are used to collimate the atomic flux toward the center of the ion trap. As the ablation process spreads atoms in every direction, a mirror and a hole in the shield are used (Fig. 17). This configuration prevents a high atomic flux from exiting the shield and directly coating the top CF-160 viewport used for the ablation laser beam. Although the mirror used for the ablation laser is directly exposed to the atomic flux produced by the ablation producing a systematic degradation on the mirror's reflectivity, this can be compensated directly by increasing the power of ablation of the laser. Additionally, there is a small square aperture in the side of the stage, which allows for monitoring of the oven temperature with a thermal camera through an infra-red

transmissive Germanium viewport. This can be used to characterize the heating dynamics of the oven in ultra-high vacuum and to optimize the loading process avoiding excess heating.<sup>95</sup>

A broad range of pulsed laser sources can produce the pulses needed for ablation. An example of such a source is a pulsed diode pumped solid state laser (DPSS), with a wavelength of 515 nm and an energy per pulse of 170  $\mu$ J.<sup>96</sup> This wavelength is compatible with our coated viewports.

## B. Vacuum preparation and ex-vacuum elements

The cleaning of all the vacuum components is done following the procedure described in Ref. 97. The main components of the vacuum chamber are pre-baked at 450 °C, whereas when adding the in-vacuum optical system and the nanopositioners, the system must be baked at 150 °C.

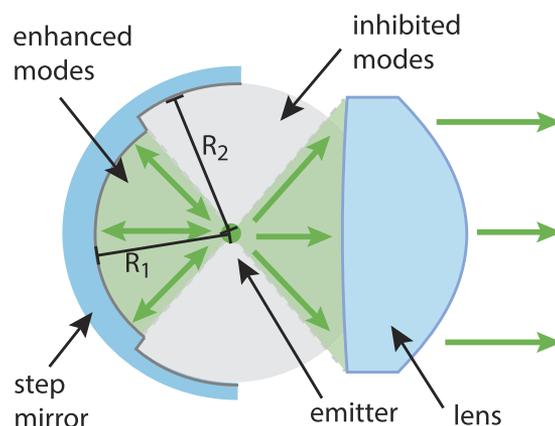
Three pairs of magnetic field coils are attached to the outside of the main chamber flanges in order to provide a homogeneous magnetic field at the center of the trap. These coils may be replaced by rings of permanent magnets in order to achieve a better suppression of RF magnetic field noise. Four legs are attached to the exterior of the vacuum chamber to support it on an optical table.

## IV. SUMMARY AND OUTLOOK

In this article, we have presented the design and construction of a new setup that will allow us to study quantum electrodynamics effects. Furthermore, the setup features an unprecedented single-mode collection efficiency. We have presented the design and construction of the main optical components of the setup, namely, a hemispherical mirror and an aspheric lens, and shown how the strict requirements on their optical performance can be fulfilled. Both the mirror and the lens achieve a wavefront distortion below  $\lambda/10$ .

The fabrication of macroscopic concave hemispherical mirrors with unprecedented precision will give us access to the enhancement and inhibition of spontaneous emission of a single atom of more than 96% of its free-space value. The fabrication technique could be extended to obtain other concave surfaces, allowing for more exotic quantum electrodynamics situations. One example would be a hemispherical mirror with a  $\lambda/4$  radius step, as shown in Fig. 18 (details can be found in Ref. 98). Such a mirror could be used to enhance spontaneous emission in the modes collected by a lens while inhibiting the rest, resulting in collection efficiencies close to 100% for a perfectly shaped mirror. For a mirror with a  $\lambda/4$  step, fabricated with the surface accuracy demonstrated in Sec. II A, combined with the NA = 0.7 lens presented in Sec. II B, an unprecedented 68.5% single-mode collection efficiency is expected for a linear dipole oriented perpendicular to the optical axis, in comparison with the 31.7% expected with a non-stepped mirror.<sup>54</sup>

We have also presented the design of a monolithic high-optical access ion trap. Such a trap provides the optical access required for the observation of the quantum electrodynamics effects described above. The trapping parameters are similar to those in state-of-the-art macroscopic traps, such as our “Innsbruck-style” blade trap.<sup>70</sup> The design of this new trap employs 3D-printing technologies. The basic concept of using trenches to separate electrodes can be extended to more complex trap geometries, including segmented traps or traps designed for trapping 2D or 3D ion crystals, with



**FIG. 18.** Step mirror concept. A mirror with the radius of curvature  $R_1 = n\lambda/2$  around the center and  $R_2 = n\lambda/2 + \lambda/4$  in the periphery would enhance emission of photons in the solid angle collected by the lens while inhibiting emission of uncollected light.

high-optical access to the trapped particles. The trap fabrication process does not require the alignment of different parts or shadow masking, which makes it reliable and repeatable. The exceptionally high-optical access achieved by the trap could also be used in ion setups that integrate an optical cavity.<sup>99,100</sup>

We have also presented the design of the complete setup, which includes a state-of-the-art vacuum vessel and an assembly for fast loading of ions in the trap via laser ablation. With several of these setups, one could perform experiments related to remote entanglement distribution and quantum networking without optical cavities.<sup>45,46</sup>

The physical phenomena that we aim to study with this setup, such as strong inhibition and enhancement of spontaneous emission, are not restricted to atomic ions but could be observed from any quantum emitter. The optical setup presented here could be used with other systems with promising prospects in quantum networking and communications, such as quantum dots or diamond spin qubits.<sup>101,102</sup>

## SUPPLEMENTARY MATERIAL

The [supplementary material](#) includes a STEP file with the trap design. This file can be opened with any standard CAD software such as SolidWorks, AutoCAD, or SALOME. Additionally, we include a 3D PDF with a 3D view of the trap. For a proper view of this file, we recommend using Adobe Acrobat Reader.

## ACKNOWLEDGMENTS

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teams for their advice and collaboration. We thank Lukas Slodicka, Martin Van Mourik, Pavel Hrmo, Ezra Kassa, Simon Ragg, and Chiara Decaroli for fruitful discussions. This work was supported by the European Commission through Project No. PIEDMONS 801285 and by the Institut für Quanteninformation GmbH. This work was also supported by the European Commission through the Marie Skłodowska-Curie Action under Grant No. 801110 (Erwin Schrödinger Quantum Fellowship Programme).

## DATA AVAILABILITY

The data that support the findings of this study are available from the corresponding author upon reasonable request.

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- <sup>76</sup>Accu-Glass male gold pins type T-2, part number 110008.
- <sup>77</sup>Lead-free solid wire solder, Harris SB61/2POP, 96% Tin, 4% Silver, 430 F.
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